

# Two-dimensional flow in a porous medium with general anisotropy

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# Darcy's law for flow in an isotropic porous medium

$$\mathbf{0} = -\nabla p - \frac{\mu}{K} \vec{v}$$

$p$  is pressure  
 $\mu$  is dynamic viscosity  
 $K$  is permeability  
 $v$  is velocity (vector)

Henry Darcy (1856) formulated this linear law where a driving force is balanced by a resistance. Analogous linear constitutive laws are:

Ohm's law of electric conduction

Fourier's law of heat conduction

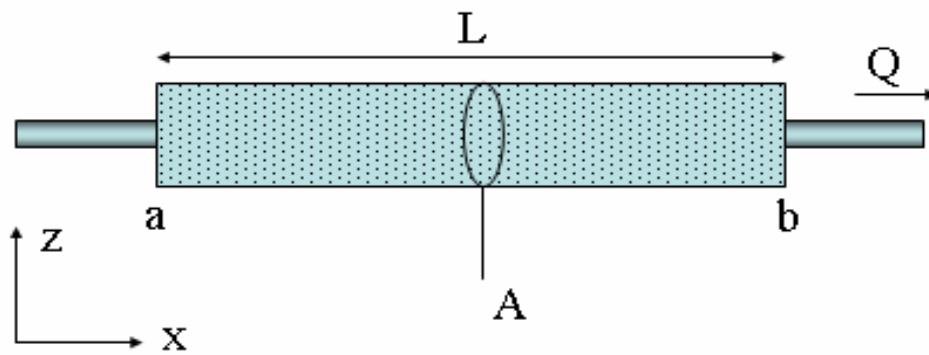
Fick's law of mass diffusion

Essentially these are first-order Taylor expansions

# Darcy's law for flow in an isotropic porous medium: Newton's 2. law

$$0 = -\nabla p - \frac{\mu}{K} \vec{v}$$

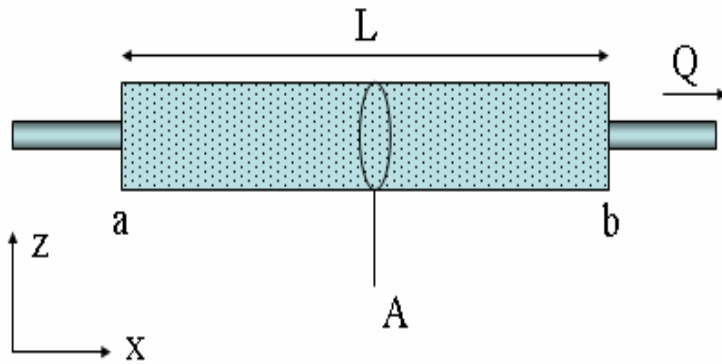
mass x acceleration = pressure force + resistance force (taken per volume, with acceleration term neglected)



Basic experiment for obtaining Darcy's law



# Basic 1D experiment for obtaining Darcy's law



Tube (a)-(b) filled with a porous medium. Pressure fall  $\Delta p = p_a - p_b$ . Tube length  $L$ . Cross-section area  $A$ . Volume flux  $Q$ .

$$Q = K \frac{A}{\mu} \frac{p_a - p_b}{L} = -K \frac{A}{\mu} \frac{\partial p}{\partial x}$$

This is the observed relationship between pressure fall and volume flux. The permeability  $K$  is introduced as a proportionality constant.

# Darcy's law for flow in an isotropic porous medium

$$0 = -\nabla p - \frac{\mu}{K} \vec{v}$$

$p$  is pressure  
 $\mu$  is dynamic viscosity  
 $K$  is permeability  
 $v$  is velocity (vector)

Follows by generalizing to 3D the empirical relationship

$$Q = K \frac{A}{\mu} \frac{p_a - p_b}{L} = -K \frac{A}{\mu} \frac{\partial p}{\partial x}$$

by introducing as velocity the specific flux  $v_x = Q/A$ . Alternatively one may work with the average pore velocity  $nQ/A$  ( $n$  is porosity).

# Darcy's law for 1D flow in an anisotropic porous medium

The 1D version of Darcy's law

$$Q = K \frac{A}{\mu} \frac{p_a - p_b}{L} = -K \frac{A}{\mu} \frac{\partial p}{\partial x}$$

is rewritten for an anisotropic medium as

$$v_x = \frac{Q_x}{A} = -\frac{K_{xx}}{\mu} \frac{\partial p}{\partial x}$$

where  $K_{xx}$  is the permeability for flow in the  $x$  direction as driven by a gradient in the  $x$  direction

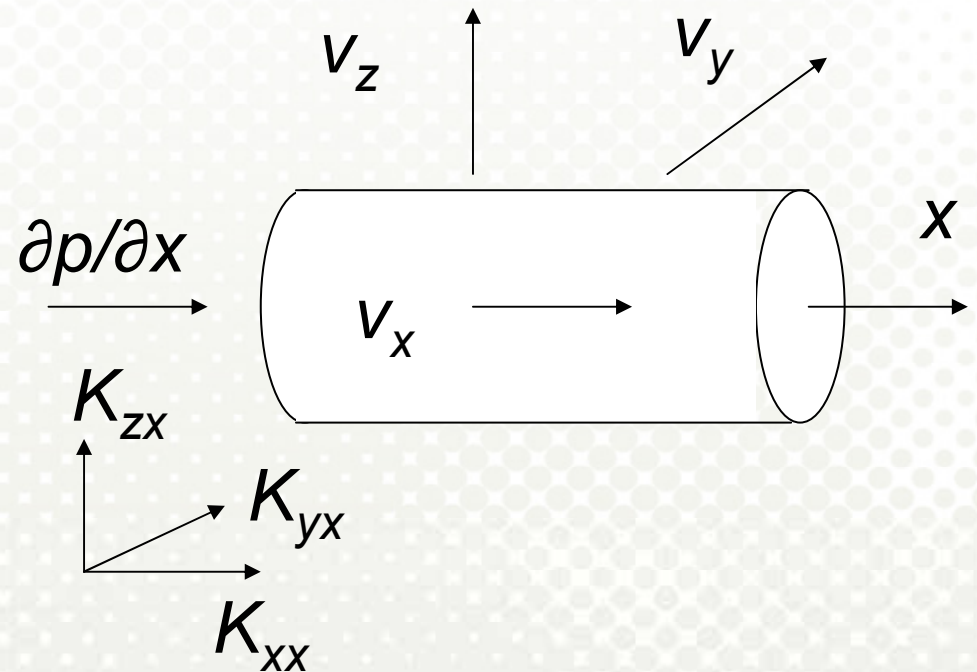
# Darcy's law for 1D flow in an anisotropic porous medium

Darcy's law for an anisotropic porous medium with 1D pressure gradient  $\partial p/\partial x = \Delta p/L_x$

$$v_x = \frac{Q_x}{A_x} = -\frac{K_{xx}}{\mu} \frac{\partial p}{\partial x}$$

$$v_y = \frac{Q_y}{A_y} = -\frac{K_{yx}}{\mu} \frac{\partial p}{\partial x}$$

$$v_z = \frac{Q_z}{A_z} = -\frac{K_{zx}}{\mu} \frac{\partial p}{\partial x}$$



$K_{yx}$ ,  $K_{zx}$  are the permeabilities for flows in the  $y$  and  $z$  directions as driven by a gradient in the  $x$  direction. Given by  $K_{yx}/K_{xx} = v_y/v_x$ ,  $K_{zx}/K_{xx} = v_z/v_x$



# Darcy's law for 3D flow in an anisotropic porous medium

Darcy's law for an anisotropic porous medium with 3D pressure gradient  $(\partial p / \partial x, \partial p / \partial y, \partial p / \partial z)$

$$\mu \begin{pmatrix} v_x & v_y & v_z \end{pmatrix} = - \begin{pmatrix} K_{11} & K_{12} & K_{13} \\ K_{21} & K_{22} & K_{23} \\ K_{31} & K_{32} & K_{33} \end{pmatrix} \begin{pmatrix} \partial p / \partial x \\ \partial p / \partial y \\ \partial p / \partial z \end{pmatrix}$$

or, in index form

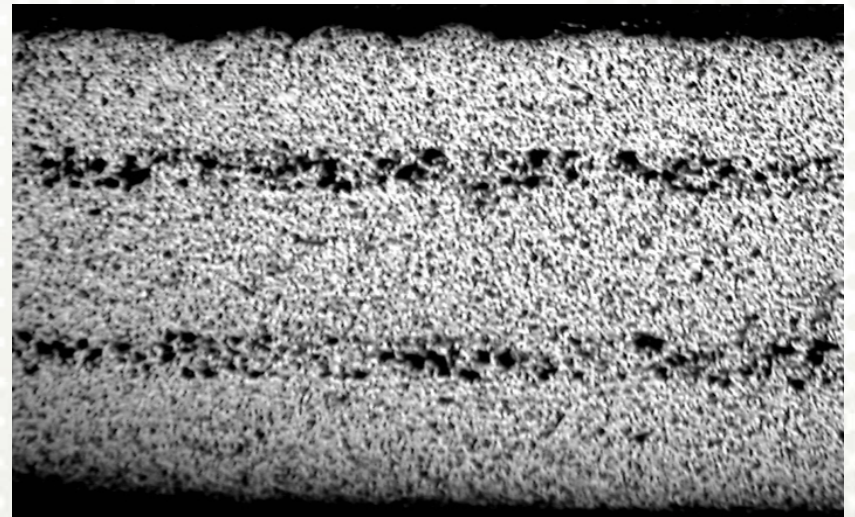
$$\mu v_i = K_{ij} \frac{\partial p}{\partial x_j}$$

$K_{ij}$  ( $i=1,2,3$ ) ( $j=1,2,3$ ) are the permeabilities for flow in the  $x_1=x$ ,  $x_2=y$  and  $x_3=z$  directions as driven by gradients in the  $x_j$  ( $j=1,2,3$ ) directions



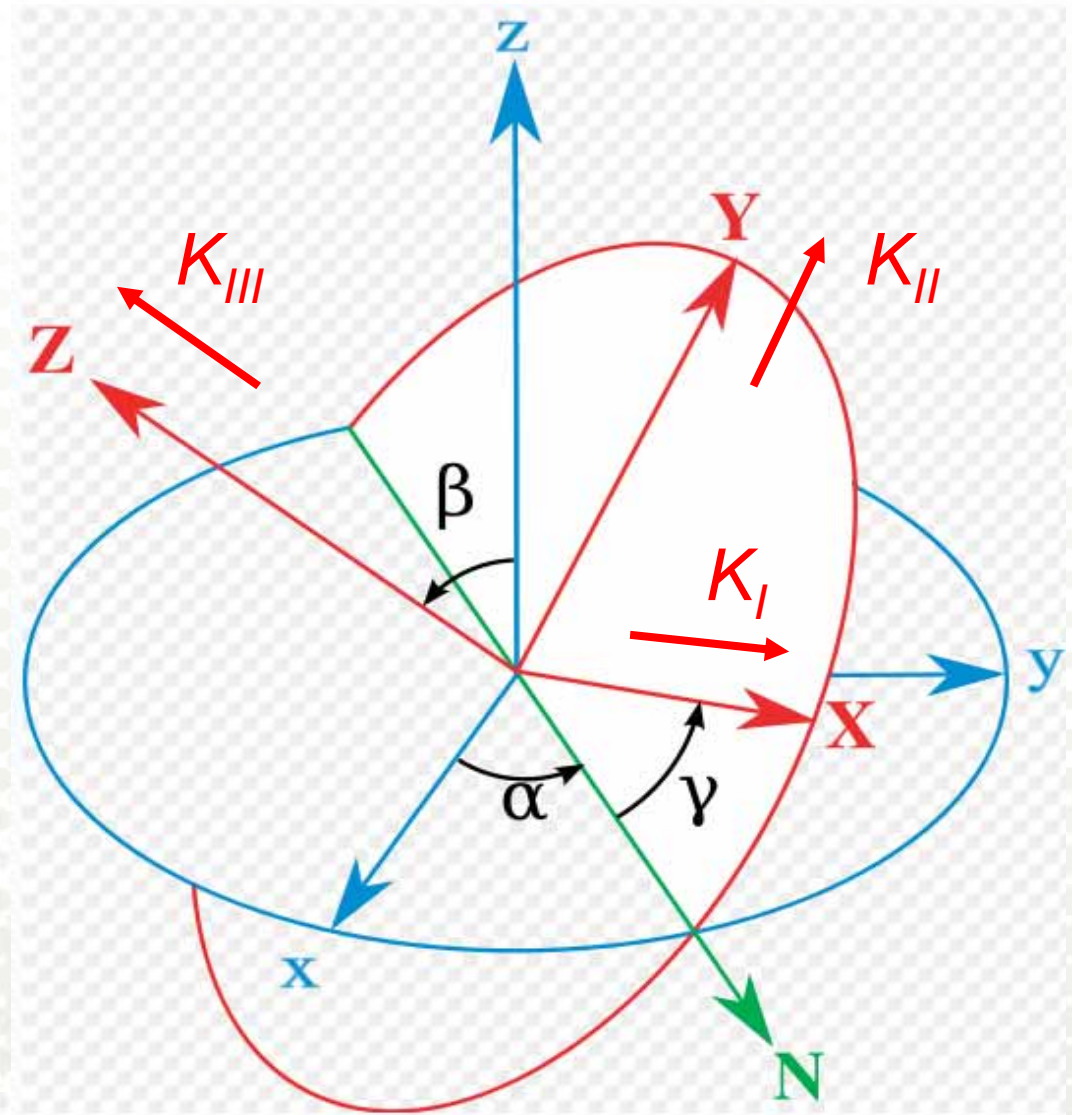
# 3D anisotropic porous media

- We consider a homogeneous porous medium with general 3D anisotropy
- The anisotropy can be caused by fibres with preferred directions
- The anisotropy can be caused by periodic layering
- These cases may have transverse isotropy:  
permeability along  
across layer.  
permeability in  
perpendicular direction
- Our analysis will assume general anisotropy, with arbitrary directions of principal axes



# Flow in a 3D anisotropic porous medium

Coordinate axes  $x, y, z$ . Principal axes of permeability  $X, Y, Z$ , with permeabilities  $K_I, K_{II}, K_{III}$ . The two coordinate systems are linked by the three Euler angles  $\alpha, \beta, \gamma$



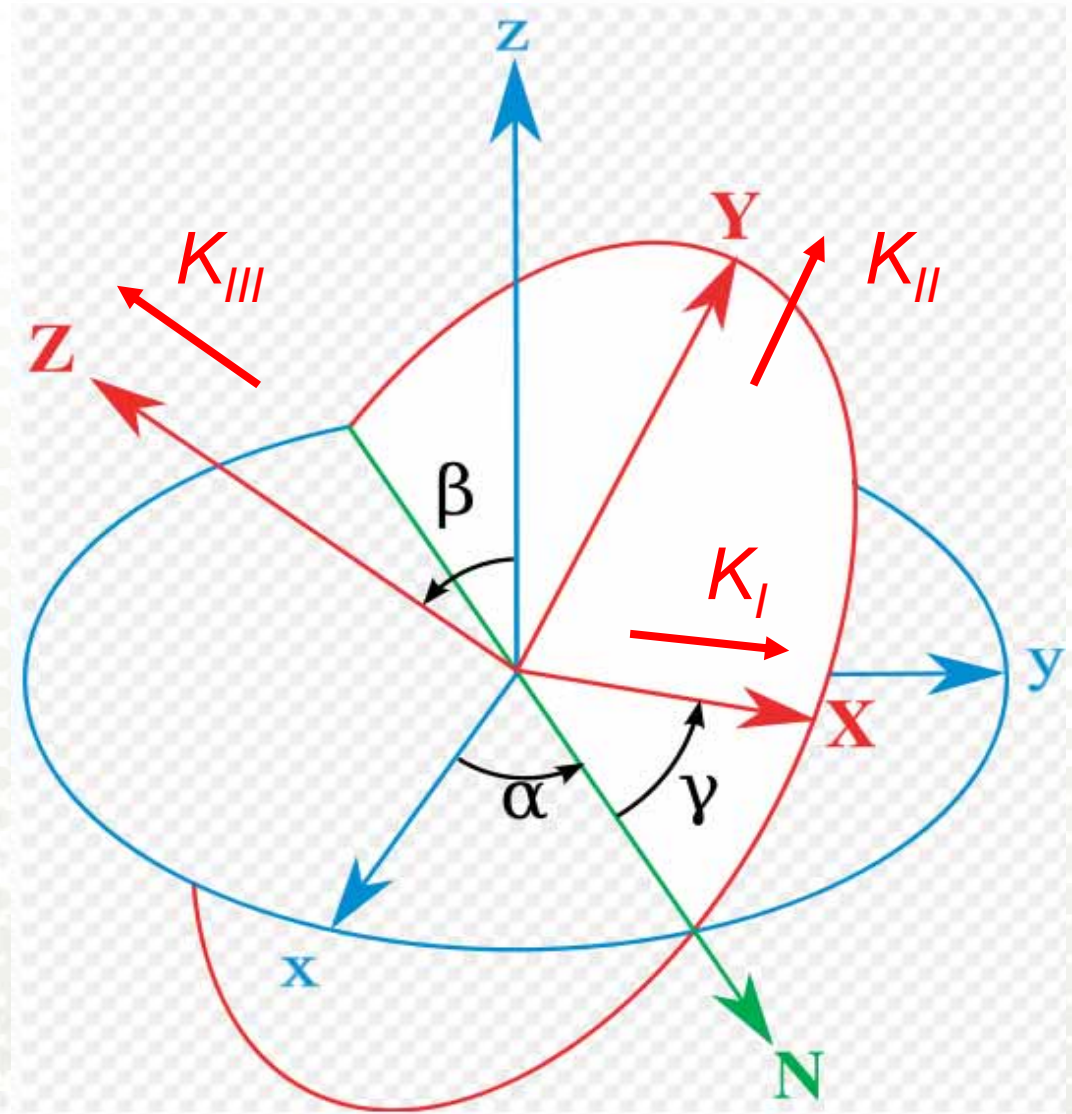


# Flow in a 3D anisotropic porous medium

Principal axes of permeability are  $X, Y, Z$ . The permeability matrix is

$$\begin{pmatrix} K_I & 0 & 0 \\ 0 & K_{II} & 0 \\ 0 & 0 & K_{III} \end{pmatrix}$$

in the  $X, Y, Z$  system. The matrix is transformed to the  $x, y, z$  system





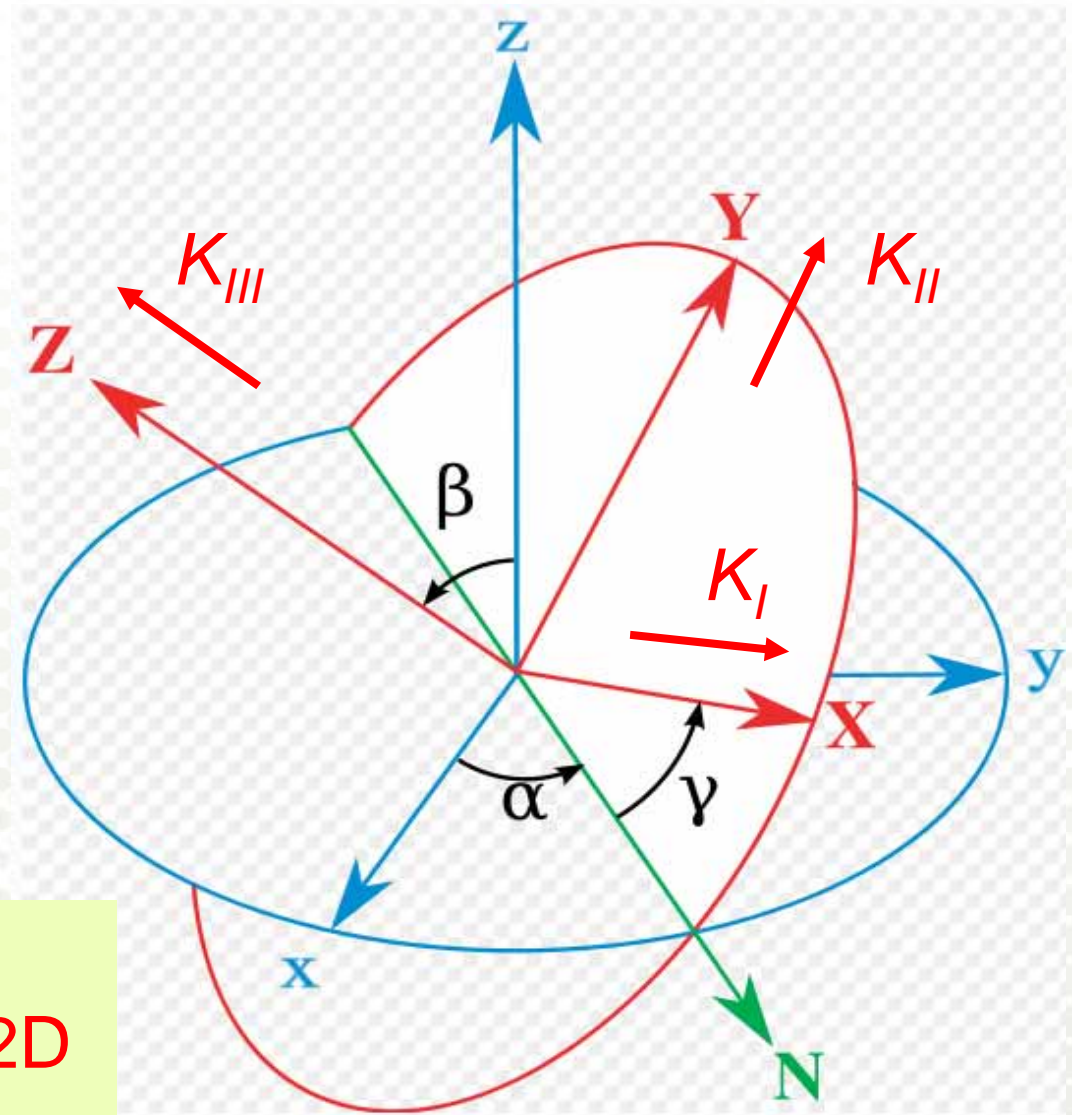
# 2D flow in a 3D anisotropic porous medium

The permeability matrix in the  $x,y,z$  system

$$\begin{pmatrix} K_{11} & K_{12} & K_{13} \\ K_{21} & K_{22} & K_{23} \\ K_{31} & K_{32} & K_{33} \end{pmatrix}$$

is given by the three principal permeabilities and the Euler angles (formulas omitted)

Now we restrict our attention to general 2D flow ( $\partial/\partial z=0$ )



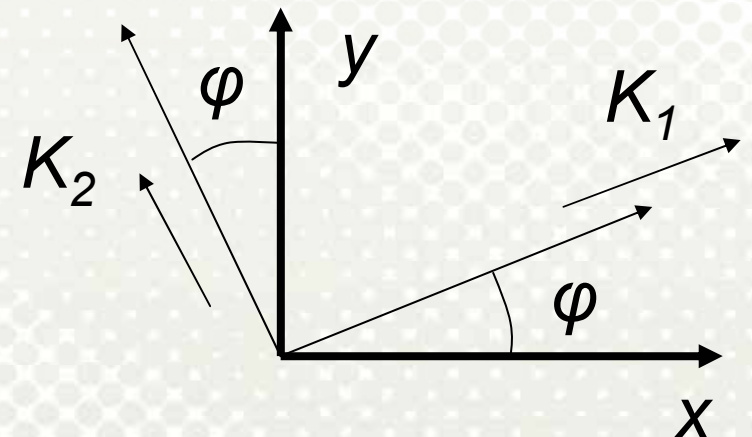
# 2D flow in a 3D anisotropic porous medium

- We introduce the pressure gradient that drives a 2D flow  $(G_x, G_y) = -(\partial p/\partial x, \partial p/\partial y)$
- Note that this flow has a passive component in the  $z$  direction, even though there is no pressure gradient in the  $z$  direction
- Darcy's law for the 3D porous medium is written as

$$\vec{v} = \underline{K} \cdot \vec{G} = \vec{G} \cdot \underline{K}$$

- Here  $K$  is the 3D permeability tensor (matrix), which is symmetric. The velocity vector  $v$  has three components  $(v_x, v_y, v_z)$

The idea is now to introduce an effective 2D description for the flow in the  $(x,y)$  plane.  $K_1$  and  $K_2$  are defined as effective 2D principal permeabilities, with axes rotated an angle  $\varphi$  compared with the coordinate axes  $x$  and  $y$



# 2D flow in a 3D anisotropic porous medium

- Darcy's law for 2D flow in a 3D porous medium with  $(G_x, G_y) = (-\partial p/\partial x, -\partial p/\partial y)$

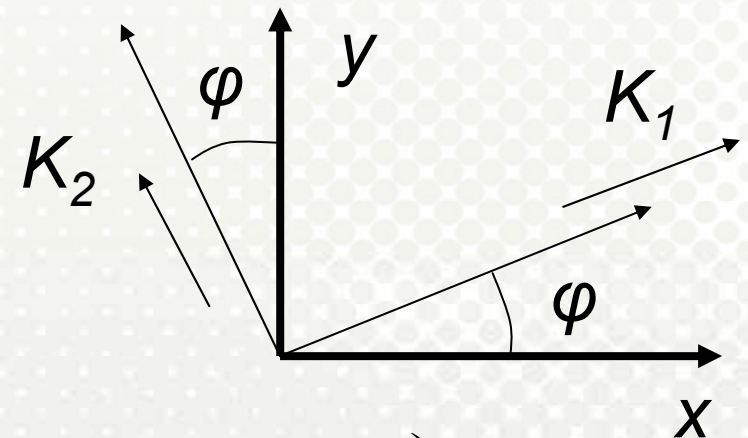
- $$\vec{v} = \underline{\underline{K}} \cdot \vec{G} = \vec{G} \cdot \underline{\underline{K}}$$

- The velocity vector  $v$  has three components  $(v_x, v_y, v_z)$ , but we are only interested in its 2D projection  $(v_x, v_y)$ , which is given by the 2D formula

$$(v_x, v_y) = \vec{G} \cdot \underline{\underline{K}}_{eff}$$

$$\underline{\underline{K}}_{eff} = \begin{pmatrix} K_1 \cos^2 \varphi + K_2 \sin^2 \varphi & (1/2)(K_1 - K_2) \sin 2\varphi \\ (1/2)(K_1 - K_2) \sin 2\varphi & K_1 \sin^2 \varphi + K_2 \cos^2 \varphi \end{pmatrix}$$

An effective 2D description for the flow in the  $(x,y)$  plane takes  $K_1$  and  $K_2$  as effective 2D principal permeabilities, with axes rotated an angle  $\varphi$





# 2D flow in a 3D anisotropic porous medium

- The equations governing  $K_1$ ,  $K_2$  and  $\varphi$  are shown here. They can easily be solved numerically.

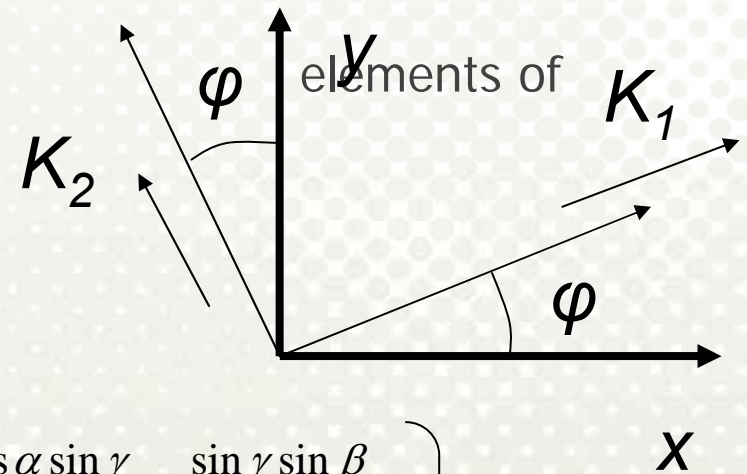
$$K_1 \cos^2 \varphi + K_2 \sin^2 \varphi = K_I a_{11}^2 + K_{II} a_{21}^2 + K_{III} a_{31}^2$$

$$K_1 \sin^2 \varphi + K_2 \cos^2 \varphi = K_I a_{12}^2 + K_{II} a_{22}^2 + K_{III} a_{32}^2$$

$$(1/2)(K_1 - K_2) \sin 2\varphi = K_I a_{11} a_{12} + K_{II} a_{21} a_{22} + K_{III} a_{31} a_{32}$$

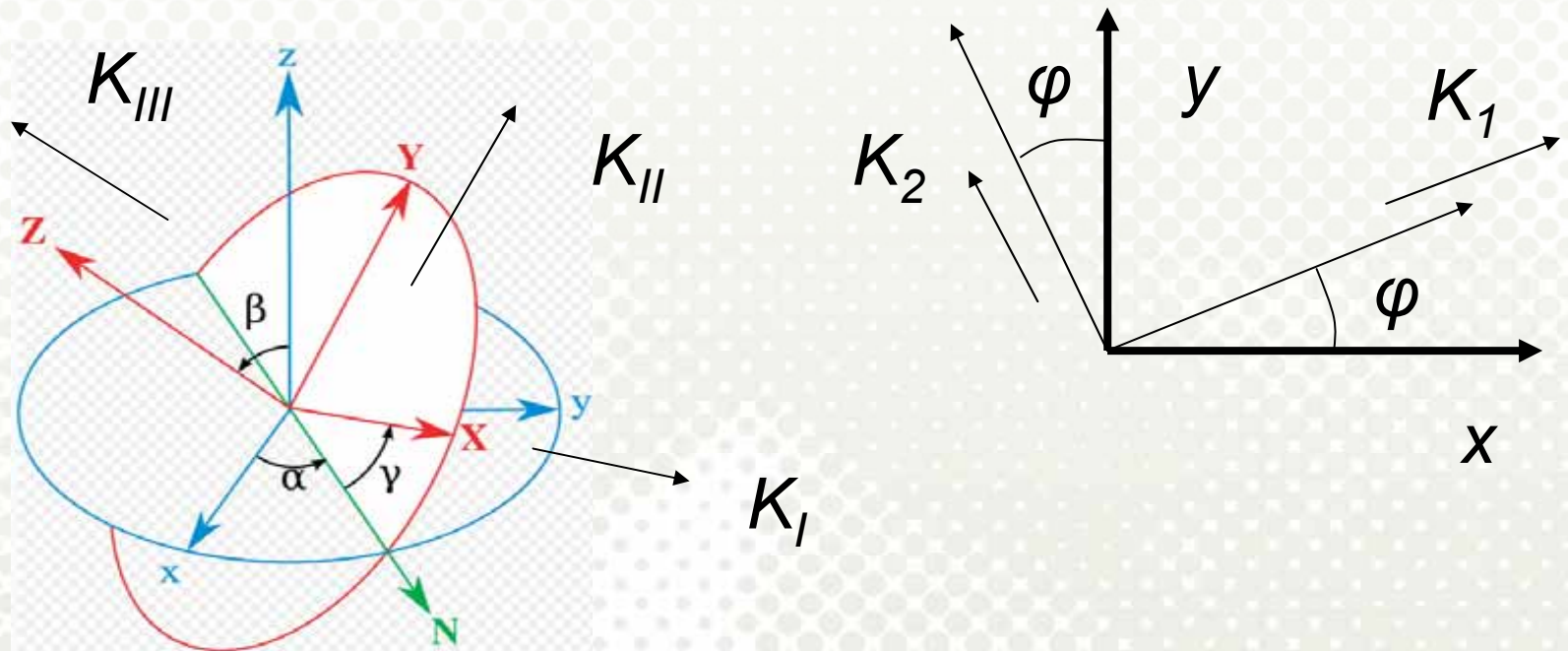
- The coefficients consist of products of the rotation matrix

$$\begin{pmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{pmatrix} = \begin{pmatrix} \cos \gamma \cos \alpha - \cos \beta \sin \alpha \sin \gamma & \cos \gamma \sin \alpha + \cos \beta \cos \alpha \sin \gamma & \sin \gamma \sin \beta \\ -\sin \gamma \cos \alpha - \cos \beta \sin \alpha \cos \gamma & -\sin \gamma \sin \alpha + \cos \beta \cos \alpha \cos \gamma & \cos \gamma \sin \beta \\ \sin \beta \sin \alpha & -\sin \beta \cos \alpha & \cos \beta \end{pmatrix}$$



## Numerical results for $K_I=1, K_{II}=2, K_{III}=3$

$\alpha$	$\beta$	$\gamma$	$\varphi$	$K_1$	$K_2$
$\pi/6$	0	$\pi/6$	$\pi/3$	1	2
$\pi/6$	$\pi/6$	$\pi/6$	.896	1.103	2.209
$\pi/6$	$\pi/3$	$\pi/6$	.670	1.218	2.719



## Numerical results for $K_I=3, K_{II}=2, K_{III}=1$

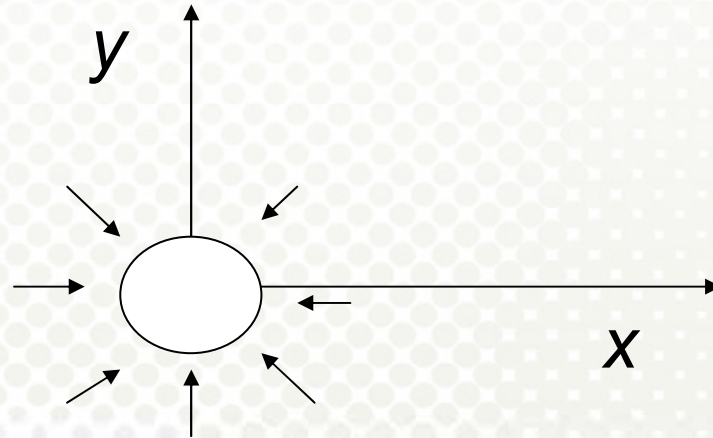
$\alpha$	$\beta$	$\gamma$	$\varphi$	$K_1$	$K_2$
$\pi/6$	0	$\pi/4$	$5\pi/12$	3	2
$\pi/6$	$\pi/8$	$\pi/4$	1.192	2.865	1.916
$\pi/6$	$\pi/4$	$\pi/4$	0.902	2.640	1.610
$\pi/6$	$3\pi/8$	$\pi/4$	0.669	2.578	1.192

Increasing  $\beta$  from zero, we see how the effective permeabilities  $K_1$  and  $K_2$  are influenced more and more from  $K_{III}$ . The values of these effective permeabilities are between the extremal 3D values



# Original motivation for this work

- We investigated drainage flow from a 2D anisotropic porous medium into a ditch. General 2D permeability matrix



$$\begin{pmatrix} K_{xx} & K_{xy} \\ K_{yx} & K_{yy} \end{pmatrix}$$

- Our question was: Will our 2D drainage theory for a uniformly draining ditch be valid for a class of porous media with 3D anisotropy? The answer is yes. It is valid for general 3D anisotropy, defining the effective 2D permeability matrix presented here

# Summary and conclusions

- A 2D flow in a general 3D anisotropic porous medium does not involve all **six** independent components of the full permeability tensor (matrix). It involves **five**, and reduces them to **three**.
- **Three** independent components of an effective 2D permeability tensor are sufficient to describe the 2D flow in the plane. These three are expressed by the principal values  $K_1$ ,  $K_2$  and the tilt angle  $\varphi$  of the principal axes.
- One disadvantage with this approach is that it overlooks the passive flow perpendicular to the  $x,y$  plane of the 2D flow
- Another disadvantage is that we cannot reconstruct the full permeability tensor. Even if we took the passive flow components into account, we only have 5 equations to determine the 6 independent tensor components. The single tensor component that we cannot find with 2D flow is  $K_{zz}$

# APPENDIX: Mathematica program for calculating the effective permeability matrix

```

Mathematica 5.2 - [dalen.nb *]
File Edit Cell Format Input Kernel Find Window Help

dalen.nb *

In[1]:= a11 = Cos[α] Cos[γ] - Sin[α] Sin[γ] Cos[β]

In[2]:= a12 = Sin[α] Cos[γ] + Cos[α] Sin[γ] Cos[β]

In[3]:= a13 = Sin[β] Sin[γ]

In[4]:= a21 = -Cos[α] Sin[γ] - Sin[α] Cos[γ] Cos[β]

In[5]:= a22 = -Sin[α] Sin[γ] + Cos[α] Cos[γ] Cos[β]

In[6]:= a23 = Sin[β] Cos[γ]

In[7]:= a31 = Sin[α] Sin[β]

In[8]:= a32 = -Cos[α] Sin[β]

In[9]:= a33 = Cos[β]

In[10]:= f[k1_, k2_, φ_] := k1 Cos[φ]^2 + k2 Sin[φ]^2 - kI a11^2 - kII a21^2 - kIII a31^2

In[11]:= g[k1_, k2_, φ_] := k1 Sin[φ]^2 + k2 Cos[φ]^2 - kI a12^2 - kII a22^2 - kIII a32^2

In[12]:= h[k1_, k2_, φ_] := (1/2) (k1 - k2) Sin[2 φ] - kI a11 a12 - kII a21 a22 - kIII a31 a32

In[13]:= ff = kI a11^2 + kII a21^2 + kIII a31^2

In[14]:= gg = kI a12^2 + kII a22^2 + kIII a32^2

In[15]:= hh = kI a11 a12 + kII a21 a22 + kIII a31 a32

In[16]:= k1[φ_] := (ff + gg) / 2 + hh / Sin[2 φ]

In[17]:= k2[φ_] := (ff + gg) / 2 - hh / Sin[2 φ]

In[18]:= los[φ_] := k1[α] Cos[φ]^2 + k2[α] Sin[φ]^2 - ff

In[29]:= kI = 1

In[30]:= kII = 2

In[31]:= kIII = 3

```

$$K_{eff} = \begin{pmatrix} K_1 \cos^2 \varphi + K_2 \sin^2 \varphi & (1/2)(K_1 - K_2) \sin 2\varphi \\ (1/2)(K_1 - K_2) \sin 2\varphi & K_1 \sin^2 \varphi + K_2 \cos^2 \varphi \end{pmatrix}$$

